

## DYNAMIC BEHAVIOR OF NONUNIFORM FUNCTIONALLY GRADED EULER-BERNOULLI BEAMS UNDER MULTIPLE MOVING FORCES

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**Abstract.** The dynamic behavior of nonuniform Euler-Bernoulli beams made of transversely functionally graded material under multiple moving forces is studied by the finite element method. The beam cross-section is assumed to vary in the width direction by two different types. A simple finite element formulation, accounting for variation of the material properties through the beam thickness and the shift in the physically neutral surface, is derived and employed in the study. The exact variation of the cross-sectional profile is employed in evaluation of the element stiffness and mass matrices. The dynamic response of the beam is computed with the aid of the implicit Newmark method. The numerical results show that the derived finite element formulation is capable to assess accurately the dynamic characteristics of the beam by using just several elements. The effect of the moving speed, material inhomogeneity and section profile on the dynamic behavior of the beams is investigated. The influence of the distance between the forces as well as the number of forces on the dynamic response is also examined and highlighted.

**Keywords:** Functionally graded beam, physically neutral surface, moving force, dynamic behavior, finite element method.

### 1. INTRODUCTION

Functionally graded materials (FGMs) have received much attention from engineers and researchers since they were first initiated by Japanese scientists in 1984 [1]. FGMs are produced by continuously varying volume fraction of constituent materials, usually ceramics and metals, in one or more spatial directions. As a result, the effective properties of FGMs exhibit continuous change, thus eliminating interface problems and mitigating thermal stress concentrations. Many investigations on analysis of FGM structures subjected to different loadings are summarized in [2,3], only contributions that are most relevant to the present work are briefly discussed below.

Chakraborty et al. [4] proposed a first-order shear deformable beam element for analyzing the thermo-elastic behavior of FGM beams. In [5], the wave propagation behavior of FGM beams under high frequency impulse loading was studied by using the spectral finite element method. Benatta et al. [6] derived an analytical solution to the bending problem of an FGM beam taking the warping effect into consideration. Based on the third-order shear deformation beam theory, Kadoli et al. [7] proposed a beam element for studying the static behavior of FGM beams under ambient temperature. Lee et al. [8] presented a finite element procedure for computing the post-buckling response of FGM plates under compressive and thermal loads. Alshorbagy et al. [9], Shahba et al. [10, 11] derived beam finite elements for studying the free vibration of beams made of transversely and axially FGMs. Based on the concept of isogeometric analysis proposed by Hughes et al. [12], Tran et al. [13], Nguyen-Xuan et al. [14] developed the isogeometric finite element formulations for static, dynamic and buckling analysis of FGM plates. The formulations utilized B-splines or non-uniform rational B-splines (NURBS) functions which enables to achieve easily the smoothness with arbitrary continuity order. Nguyen [15, 16], Nguyen and Gan [17] formulated nonlinear beam finite elements for investigating the large displacement behavior of tapered beams composed of axially and transversely FGMs. In [18] Nguyen et al. presented a finite element procedure for geometrically nonlinear analysis of planar FGM beam and frame structures.

The problems of moving loads on an elastic beam are often met in the design of bridges, railways, highways... and they are subject of investigation for a long time. Both analytical method [16–18], and finite element method [19–22] are extensively employed in solving the moving load problems. With the rapid development and application of FGMs, analysis of FGM beams subjected to moving loads has been drawn attention from researchers recently. Şimşek and Kocatürk [23] employed polynomials to approximate the displacement variables in solving the equations of motion of a transversely FGM Euler-Bernoulli beam subjected to a moving harmonic force. Also using the method in [23], Şimşek extended his work to problems of FGM beams subjected to a moving mass [24], and a nonlinear FGM beam under a moving harmonic force [25]. Rajabi et al. [26] studied the dynamic behavior of an FGM Euler-Bernoulli beam subjected to a moving oscillator by using the Runge-Kutta in solving the equations of motion. In [27], Malekzadeh and Monajjemzadeh used the finite element method to investigate the dynamic response of an FGM plate resting on a Pasternak foundation subjected to thermal loading and a moving load. Also using the finite element method, Nguyen et al. [28] studied the vibration of a nonuniform FGM Timoshenko beam under a moving harmonic load.

It has been stressed recently that the shift of the physically neutral surface of transversely FGM beams should be taken into account for correctly predicting the behavior of the beams [29]. In this line of work, Kang and Li [30, 31] determined the neutral axis position of a nonlinear FGM Euler-Bernoulli beam and then derived the solutions for tip displacements of the beam subjected to a tip moment or a tip transverse load. Based on the neutral surface and the third-order shear deformation beam theory, Zhang [32] investigated the nonlinear bending of FGM beams. Eltaher et al. [33] considered the shift in the neutral axis position in the derivation of a beam finite element for studying the

free vibration of FGM macro/nano beams. It has been shown in [33] that the natural frequencies of an FGM beam are overestimated by ignoring the shift in the neutral axis position.

Because of the interaction between the moving forces, the dynamic response of a beam to multiple moving forces, as shown by Henchi et al. [34], is very different from that of a beam subjected to a single moving force. To the authors' best knowledge, the dynamic behavior of nonuniform FGM beams under multiple moving forces has not been studied in the literature, and it will be a subject of investigation of the present work. To this end, the finite element method previously used by the first two authors and their co-worker in Ref. [28], is again employed herein. The beam cross-section is assumed to vary in the width direction in two different manners. A finite element formulation, taking the variation of the elastic properties through the thickness and the shift in the physically neutral surface into account, is derived and employed in the study. It should be noted that in regard of the work by Şimşek and Kocatürk [23], two different features are considered in the present work. Firstly, the longitudinal variation of the beam cross-section is the one which is not easy to handle by the analysis method used in [23]. Secondly, the multiple moving forces, which has not been considered in [23] and in our previous work [28], requires some effort in numerical treatment. The dynamic response of the beam such as the time histories for mid-span deflection, dynamic deflection factor and axial stress distribution through the thickness are computed with the aid of the direct integration Newmark method. The effect of the material inhomogeneity, section parameter and moving speed on the dynamic behavior of the beam is investigated in detail. The influence of the material inhomogeneity, section profile and well as the loading parameters on the dynamic behavior of the beams is also examined and highlighted.

## 2. PROBLEM STATEMENT

Fig. 1 shows a simply supported beam with length  $L$ , width  $b$ , height  $h$ , subjected to  $N$  forces  $P_1, P_2, \dots, P_N$ , moving at a constant speed  $v$  from left to right. In the figure, a Cartesian co-ordinate system  $(x_1, z_1)$  is introduced as that the  $x_1$ -axis lies on the bottom surface, and  $z_1$ -axis directs upward. The distance between the force,  $d$ , is considered to be constant. The area  $A$ , and moment of inertia  $I$  of the beam cross-section are assumed to vary longitudinally in two following types

$$\text{- Type A: } A = A_0 \left( 1 - \alpha \left| \frac{x}{L} - \frac{1}{2} \right| \right), \quad I = I_0 \left( 1 - \alpha \left| \frac{x}{L} - \frac{1}{2} \right| \right),$$

$$\text{- Type B: } A = A_0 \left[ 1 - \alpha \left( \frac{x}{L} - \frac{1}{2} \right)^2 \right], \quad I = I_0 \left[ 1 - \alpha \left( \frac{x}{L} - \frac{1}{2} \right)^2 \right],$$

where  $A_0$  and  $I_0$  denote the area and moment of inertia of the mid-span cross-section, respectively;  $0 \leq \alpha < 2$  is the nonuniform section parameter. When  $\alpha = 0$ , the beam becomes uniform. The two types of the section profile are depicted in the lower part of Fig. 1.

The beam material is assumed to be composed of metal and ceramic phases whose volume fraction varies in the transverse direction according to

$$V_c = \left(\frac{z_1}{h}\right)^n, \quad V_c + V_m = 1, \quad (1)$$

where  $V_c, V_m$  are the volume fractions of ceramic and metal, respectively;  $n$  is the grading index, governing variation of the material properties through the beam thickness. As seen from Eq. (1), the bottom surface contains only metal and the top surface is pure ceramic. The composition is metal rich when  $n < 1$ , and metal poor when  $n > 1$ .

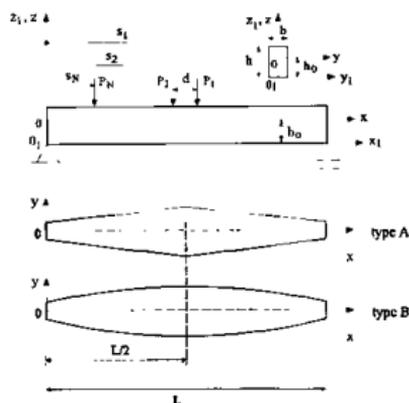


Fig. 1. Nonuniform FGM beam under multiple moving forces

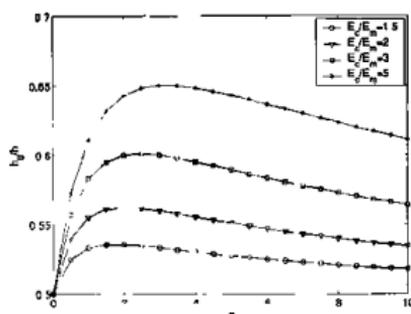


Fig. 2. Dependence of neutral surface position on the index  $n$

The effective material properties (such as Young's modulus and mass density),  $\mathcal{P}$ , can be evaluated by a simple rule

$$\mathcal{P}(z_1) = \mathcal{P}_c V_c + \mathcal{P}_m V_m = (\mathcal{P}_c - \mathcal{P}_m) \left(\frac{z_1}{h}\right)^n + \mathcal{P}_m, \quad (2)$$

where  $\mathcal{P}_m$  and  $\mathcal{P}_c$  are the properties of metal and ceramic, respectively.

Clearly, due to the variation of the Young's modulus  $E$  in the thickness direction, the neutral surface of the FGM beam does not coincide with the mid-plane. Denoting  $h_0$  as distance from the neutral surface to the bottom surface, and by introducing a new co-ordinate system  $(x, z)$  with the  $x$ -axis lies on the neutral surface, and  $z$ -axis directs upward as depicted in Fig. 1, the position of the neutral surface can be determined by using equilibrium condition for the beam subjected to pure bending as [29]

$$\int_A \sigma dA = \frac{b(x)}{\rho} \int_{-h_0}^{h-h_0} z E(z) dz = 0, \quad (3)$$

where  $\sigma$  is the axial stress for the beam in pure bending, and  $\rho$  is the curvature radius of the neutral surface. Substituting  $z = (z_1 - h_0)$  into Eq. (3), the position of the neutral

surface can be determined with the aid of Eq. (2) as

$$h_0 = \frac{\int_0^h E(z_1)z_1 dz_1}{\int_0^h E(z_1) dz_1} = \frac{h(n+1)(2E_c + nE_m)}{2(n+2)(E_c + nE_m)}. \quad (4)$$

The dependence of the neutral surface position upon the index  $n$  according to Eq. (4) is shown in Fig. 2 for various ratios of Young's modulus of ceramic to that of metal,  $E_c/E_m$ . As seen from the figure, for  $E_c/E_m > 1$  the physical neutral surface shifts upward from the mid-plane, regardless of the index  $n$ .

Based on the Euler-Bernoulli beam theory, the displacements  $u_1, u_2, u_3$  at a point  $(x, y, z)$  in the  $x, y, z$  directions, respectively are given by

$$\begin{aligned} u_1(x, y, z, t) &= u(x, t) - zw_x(x, t), \\ u_2(x, y, z, t) &= 0, \\ u_3(x, y, z, t) &= w(x, t), \end{aligned} \quad (5)$$

where  $u(x, t)$  and  $w(x, t)$  are the axial and transverse displacements of a point on the neutral axis;  $z$  is a spatial co-ordinate in the thickness direction, and  $(\dots)_x$  denotes the derivative with respect to  $x$ . Based on the Hook's law, the axial strain  $\epsilon$ , and axial stress  $\sigma$  resulted from Eq. (5) are as follows

$$\begin{aligned} \epsilon &= u_x - zw_{xx} = u_x + z\kappa, \\ \sigma &= E(z)\epsilon = E(z)(u_x + z\kappa), \end{aligned} \quad (6)$$

where  $\kappa = -w_{xx}$  is the beam curvature.

The partial differential equations of motion for the beam under the moving forces can be derived by applying Hamilton's principle. For the sake of brevity, the damping effect of the beam is not considered in the present work. The strain energy stored in the beam resulted from Eq. (6) has the following simple form

$$U = \frac{1}{2} \int_0^L \int_{A(x)} \sigma \epsilon \, dA dx = \frac{1}{2} \int_0^L [A_{11}(x)u_x^2 - 2A_{12}(x)u_x w_{xx} + A_{22}(x)w_{xx}^2] \, dx, \quad (7)$$

in which

$$(A_{11}, A_{12}, A_{22}) = \int_{A(x)} E(z)(1, z, z^2) dA, \quad (8)$$

are the axial, axial-bending coupling and bending rigidities, respectively. It is worthy to note that in substituting  $z = z_1 - h_0$  into Eq. (8), and taking Eq. (4) into consideration, the coupling rigidity  $A_{12}$  defined by Eq. (8) vanishes. As a result, the stiffness matrix resulted from Eq. (7) contains no coupling term.

The kinetic energy of the beam resulted from the displacements (5) is as follows

$$\begin{aligned} \mathcal{T} &= \frac{1}{2} \int_0^L \int_{A(x)} \rho(z) (\dot{u}_1^2 + \dot{u}_3^2) \, dA dx \\ &= \frac{1}{2} \int_0^L [I_{11}(x)(\dot{u}^2 + \dot{w}^2) - 2I_{12}(x)\dot{u}\dot{w}_x + I_{22}(x)\dot{w}_x^2] \, dx, \end{aligned} \quad (9)$$

where a over dot indicates the derivative with respect to time  $t$ , and  $I_{11}$ ,  $I_{12}$  and  $I_{22}$  are the mass moments, defined as

$$(I_{11}, I_{12}, I_{22}) = \int_{A(x)} \rho(z)(1, z, z^2) dA, \quad (10)$$

where the mass density  $\rho(z)$  varies in the thickness direction according to Eq. (2) (with  $z = z_1 - h_0$ ). It should be noted that for the longitudinal variation of cross-section considered herein the rigidities  $A_{ij}$  and the mass moments  $I_{ij}$  depend upon  $x$ . In addition, the coupling mass moment  $I_{12}$ , unfortunately does not vanish, and thus the mass matrix contains the coupling term.

The potential energy of the moving forces is simply given by

$$V = - \sum_{i=1}^N P_i w(x, t) \delta(x - vt_i(t)), \quad (11)$$

where  $\delta(\cdot)$  is the delta Dirac function, and  $t_i$  is the time since the load  $P_i$  enters the beam from its left end.

Applying Hamilton's principle to Eqs. (7), (9) and (11), the differential equations of motion for the beam can be written in the forms

$$\begin{aligned} I_{11} \ddot{u} - I_{12} \ddot{w}_{,x} - (A_{11} u_{,x})_{,x} &= 0, \\ I_{11} \ddot{w} + (I_{12} \ddot{u})_{,x} - (I_{22} \ddot{w}_{,x})_{,x} + (A_{22} w_{,xx})_{,xx} &= \sum_{i=1}^N P_i \delta(x - vt_i). \end{aligned} \quad (12)$$

Except for the presence of the coupling mass moment  $I_{12}$ , the system of equations (12) has the same forms as that of a nonuniform homogeneous beam.

### 3. FINITE ELEMENT FORMULATION

The finite element method is employed herein to solve Eq. (12). To this end, the beam is assumed being divided into a number of two-node beam elements with length of  $l$ . There are axial and transverse displacements and a rotation at each node. Thus, the vector of nodal displacements,  $\mathbf{d}$ , for a generic element has the following components

$$\mathbf{d} = \{u_i, w_i, \theta_i, u_j, w_j, \theta_j\}^T. \quad (13)$$

where and hereafter a superscript "T" denotes the transpose of a vector or a matrix. The axial displacement  $u$  and transverse displacement  $w$  are interpolated from the nodal displacements according to

$$u = \mathbf{N}_u \mathbf{d}, \quad w = \mathbf{N}_w \mathbf{d}, \quad (14)$$

where  $\mathbf{N}_u$  and  $\mathbf{N}_w$  are the matrices of shape functions for  $u$  and  $w$ , respectively. Substituting Eq. (14) into Eqs. (7) and (9), we get

$$U = \frac{1}{2} \sum_{i=1}^{n_{el}} \mathbf{d}^T \mathbf{k} \mathbf{d} = \frac{1}{2} \sum_{i=1}^{n_{el}} \mathbf{d}^T (\mathbf{k}_{uu} + \mathbf{k}_{\theta\theta}) \mathbf{d}, \quad (15)$$

and

$$\mathcal{T} = \frac{1}{2} \sum_{i=1}^{n_{el}} \dot{\mathbf{d}}^T \mathbf{m} \dot{\mathbf{d}} = \frac{1}{2} \sum_{i=1}^{n_{el}} \dot{\mathbf{d}}^T (\mathbf{m}_{uu} + \mathbf{m}_{ww} + \mathbf{m}_{u\theta} + \mathbf{m}_{\theta\theta}) \dot{\mathbf{d}}. \quad (16)$$

In Eqs. (15) and (16),  $n_{el}$  is the total number of elements;  $\mathbf{k}$  and  $\mathbf{m}$  are respectively the element stiffness and mass matrices, and

$$\begin{aligned}\mathbf{k}_{uu} &= \int_0^l \mathbf{N}_{u,x}^T A_{11} \mathbf{N}_{u,x} dx, \\ \mathbf{k}_{\theta\theta} &= \int_0^l \mathbf{N}_{w,xx}^T A_{22} \mathbf{N}_{w,xx} dx,\end{aligned}\quad (17)$$

are respectively the stiffness matrices stemming from stretching and bending,

$$\begin{aligned}\mathbf{m}_{uu} &= \int_0^l \mathbf{N}_u^T I_{11} \mathbf{N}_u dx, \quad \mathbf{m}_{ww} = \int_0^l \mathbf{N}_w^T I_{11} \mathbf{N}_w dx \\ \mathbf{m}_{u\theta} &= \int_0^l \mathbf{N}_u^T I_{12} \mathbf{N}_{w,x} dx, \quad \mathbf{m}_{\theta\theta} = \int_0^l \mathbf{N}_{w,x}^T I_{22} \mathbf{N}_{w,x} dx\end{aligned}\quad (18)$$

are the mass matrices stemming from axial displacement, transverse displacement, axial-bending coupling and cross-section rotation, respectively.

Having the element stiffness and mass matrices derived, the finite element equation for vibration of the beam is as follows

$$\mathbf{M}\dot{\mathbf{D}} + \mathbf{K}\mathbf{D} = \mathbf{F}_{ex}, \quad (19)$$

where  $\mathbf{M}, \mathbf{K}$  are the structural mass and stiffness matrices assembled from the element mass and stiffness matrices, respectively;  $\mathbf{F}_{ex}$  is the structural nodal load vector of the external forces with the following form

$$\mathbf{F}_{ex} = \left\{ \begin{array}{cccccccc} 0 & \dots & \underbrace{P_1 \mathbf{N}_w|_{x_1}}_{\text{loading element}} & 0 & \dots & 0 & \underbrace{P_i \mathbf{N}_w|_{x_i}}_{\text{loading element}} & 0 & \dots & \underbrace{P_N \mathbf{N}_w|_{x_N}}_{\text{loading element}} & 0 & \dots & 0 \end{array} \right\}^T, \quad (20)$$

which contains all zero coefficients, except for the elements currently under loading. The notation  $\mathbf{N}_w^T|_{x_i}$  in the above equation implies that the shape functions  $\mathbf{N}_w$  are evaluated at the abscissa  $x_i$ , the current position of load  $P_i$ .

The system of equations (19) can be solved by the direct integration Newmark method. The average acceleration implicit Newmark method described in [35], which ensures the unconditional convergency is adopted in the present work. In the free vibration analysis, the right hand side of Eq. (19) is set to zeros, and a harmonic response,  $\mathbf{D} = \hat{\mathbf{D}} \sin \omega t$  is assumed, so that Eq. (19) deduces to

$$(\mathbf{K} - \omega^2 \mathbf{M})\hat{\mathbf{D}} = 0, \quad (21)$$

where  $\omega$  is the circular frequency, and  $\hat{\mathbf{D}}$  is the vibration amplitude. Eq. (21) can be solved by a standard method of the eigenvalue problem [35]. To improve the accuracy, the exact variation of the cross-sectional profiles is employed in evaluation of the rigidities and mass moments defined in Eqs. (8) and (10), respectively.

#### 4. NUMERICAL RESULTS AND DISCUSSION

A simply supported FGM beam with  $L = 20$  m,  $h = 0.8$  m,  $b_0 = 2$  m, where  $b_0$  is the width of the mid-span cross section, is employed in this Section to study the dynamic response of the beam. Steel and alumina are employed as metal and ceramic phases of the FGM, respectively. The Young's modulus and mass density are respectively  $E_m = 210$  GPa and  $\rho_m = 7800$  kg/m<sup>3</sup> for steel, and that for alumina are  $E_c = 390$  GPa and  $\rho_c = 3960$  kg/m<sup>3</sup> [23]. Unless stated, the beam is assumed under action of three moving forces with the same amplitude,  $P_1 = P_2 = P_3 = P_0 = 100$  kN.

Linear and cubic Hermite polynomials are adopted as the shape functions for the axial and transverse displacements, respectively. Thus, the matrices of shape functions  $N_u$  and  $N_w$  in Eq. (14) have the following forms

$$\begin{aligned} N_u &= \{N_{u1} \ 0 \ 0 \ N_{u2} \ 0 \ 0\}, \\ N_w &= \{0 \ N_{w1} \ N_{w2} \ 0 \ N_{w3} \ N_{w4}\}, \end{aligned} \quad (22)$$

in which

$$\begin{aligned} N_{u1} &= \frac{l}{l} x, \quad N_{u2} = \frac{x}{l}, \\ N_{w1} &= 2\frac{x^3}{l^3} - 3\frac{x^2}{l^2} + 1, \quad N_{w2} = \frac{x^3}{l^2} - 2\frac{x^2}{l} + x, \\ N_{w3} &= -2\frac{x^3}{l^3} + 3\frac{x^2}{l^2}, \quad N_{w4} = \frac{x^3}{l^2} - 2\frac{x^2}{l}. \end{aligned} \quad (23)$$

For the case of constant moving speed considered herein, total time  $\Delta T$  necessary for a force to cross the beam is  $L/v$ . In the computation reported below a uniform time increment width of  $\Delta t = \Delta T/500$  is employed for the Newmark method. In order to facilitate the discussion of numerical results, the following dimensionless parameters representing the maximum mid-span dynamic deflection and the moving force speed are introduced as

$$f_D = \max \left( \frac{w(L/2, t)}{w_0} \right), \quad f_v = \frac{v}{v_{cr}^0} = \frac{\pi v}{\omega_1^0 L}, \quad (24)$$

where  $w_0 = P_0 L^3 / 48 E_m I_0$  is the static deflection of the uniform steel beam under a static load  $P_0$  acting at the mid-span;  $v_{cr}^0 = \omega_1^0 L / \pi$ , with  $\omega_1^0 = \frac{\pi^2}{L^2} \sqrt{E_m I_0 / \rho_m A_0}$ , is the critical speed of the simply supported uniform steel beam [19]. The definition of parameter  $f_D$  by Eq. (24) is similar to that of the dynamic magnification factor in the moving load problem of homogeneous beams [19]. However, for the FGM beam considered in the present work,  $f_D$  is not only governed by the moving speed but by the material inhomogeneity and the section profile also, and it will be called the dynamic deflection factor in the below.

##### 4.1. Formulation verification

In order to verify the accuracy of the derived finite element formulation, the fundamental frequency and dynamic response of a uniform FGM Bernoulli beam subjected to a moving point force are firstly computed and compared to the result of Ref. [23]. To this end, a simply supported beam with width  $b = 0.4$  m, height  $h = 0.9$  m, previously

used in Ref. [23], is adopted in this subsection. The beam is also composed of steel and alumina with the above mentioned material properties.

In Tab. 1, the fundamental frequency parameter of a uniform FGM beam with assumed properties  $E_c/E_m = 3$ ,  $\rho_c = \rho_m$  obtained by different numbers of elements is listed for various values of the index  $n$  and different length to height ratios,  $L/h = 20$  and  $L/h = 100$ . The frequency parameter  $\mu_1$  in Tab. 1 is defined as  $\mu_1 = \omega_1 L^2 \sqrt{\rho_m A/E_m I}$ , where  $A = bh$ ,  $I = bh^3/12$ , and  $\omega_1$  is the fundamental frequency of the beam. The Tab. 1 shows the fast convergency of the present formulation, and all the frequencies converge by using just ten elements. In Tab. 2, the fundamental frequency parameter is given for various values of the index  $n$ , the ratio of length to height  $L/h$ , and the ratio of Young's moduli  $E_{rat} = E_c/E_m$ . Due to the convergency stated above, only twelve elements were used in evaluating the frequencies in Tab. 2. The corresponding parameter obtained by Şimşek and Kocatürk in Ref. [23] is also listed in Tab. 2. Tab. 2 shows the good agreement between the fundamental frequencies obtained in the present work with that of Ref. [23]. In Tab. 3, the maximum dynamic deflection factor and the corresponding moving speed of the uniform FGM beam are listed for various values of the index  $n$ . For comparison purpose, the corresponding data of Ref. [23] are also given in Tab. 3. Very good agreement between the numerical result of the present work with that of Ref. [23] is noted.

Table 1. Convergncy of present formulation in evaluating fundamental frequency of a uniform FGM beam ( $\rho_c = \rho_m$ ,  $E_c/E_m = 3$ )

		$n_{el}$						
$L/h$	$n$	2	4	6	8	10	12	Ref. [23]
20	0.1	4.0555	4.0481	4.0477	4.0476	4.0476	4.0476	4.0475
	0.2	3.9820	3.9747	3.9742	3.9742	3.9741	3.9741	3.9741
	2	3.5386	3.5321	3.5317	3.5317	3.5317	3.5317	3.5308
	3	3.4935	3.4871	3.4867	3.4867	3.4867	3.4867	3.4858
	10	3.3810	3.3748	3.3745	3.3744	3.3744	3.3744	3.3738
100	0.1	4.0572	4.0497	4.0493	4.0492	4.0492	4.0492	4.0495
	0.2	3.9836	3.9763	3.9758	3.9758	3.9758	3.9758	3.9761
	2	3.5402	3.5337	3.5333	3.5333	3.5333	3.5333	3.5331
	3	3.4951	3.4887	3.4883	3.4882	3.4882	3.4882	3.4881
	10	3.3825	3.3762	3.3759	3.3758	3.3758	3.3758	3.3757

Secondary, the time history for dynamic mid-span deflection of a uniform homogeneous beam subjected to three moving forces, previously studied by Henchi et al. in Ref. [34] by the dynamic stiffness method, is computed. The beam geometric and material data are:  $L = 24.384$  m,  $A = 0.954$  m<sup>2</sup>,  $I = 2.9 \times 10^{-4}$  m<sup>4</sup>,  $E = 19 \times 10^{11}$  N/m<sup>2</sup>,

Table 2. Fundamental frequency parameter  $\mu_1$  of uniform FGM beam with assumed material properties  $\rho_c = \rho_m$  ( $E_{rat} = E_a/E_s$ )

$L/h$	$E_{rat}$	Source	$n = 0.1$	$n = 0.2$	$n = 1$	$n = 2$	$n = 3$	$n = 10$
20	2	Ref. [23]	3.6775	3.6301	3.4421	3.3765	3.3500	3.2725
		Present	3.6776	3.6303	3.4426	3.3770	3.3505	3.2729
	4	Ref. [23]	4.3370	4.2459	3.8234	3.6485	3.5858	3.4543
		Present	4.3370	4.2459	3.8243	3.6496	3.5870	3.4551
100	2	Ref. [23]	3.6793	3.6320	3.4440	3.3784	3.3519	3.2742
		Present	3.6791	3.6318	3.4440	3.3784	3.3519	3.2743
	4	Ref. [23]	4.3392	4.2481	3.8259	3.6513	3.5886	3.4565
		Present	4.3388	4.2476	3.8260	3.6514	3.5887	3.4566

Table 3. Maximum dynamic deflection factor and corresponding moving speed of uniform FGM beam under a single moving force

$n$	$\max(f_D)$		$v$ (m/s)	
	Present	Ref. [23]	Present	Ref. [23]
0.2	1.0347	1.0344	222	222
0.5	1.1445	1.1444	197	198
1	1.2504	1.2503	179	179
2	1.3377	1.3376	164	164
pure steel	1.7326	1.7324	132	132
pure alumina	0.9329	0.9328	252	252

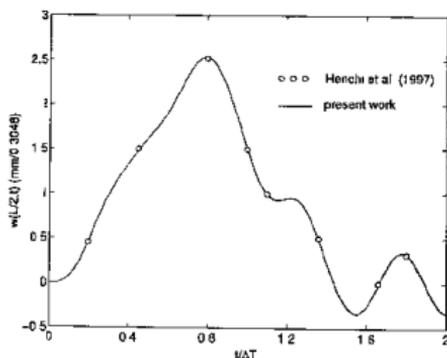


Fig. 3. Dynamic mid-span deflection of uniform homogeneous beam under three moving forces ( $d = L/4$ ,  $v = 22.5$  m/s)

$\rho A = 9.576 \times 10^3 \text{ kg/m}^3$ , where  $L, A, I, E, \rho$  are the total length, cross-sectional area, moment of inertia of cross-section, Young's modulus and mass density of the beam, respectively. Fig. 3 shows the mid-span dynamic deflection for the case  $P_0 = 5324.256 \text{ N}$ ,  $v = 22.5 \text{ m/s}$ ,  $d = L/4$ , where the numerical result obtained by Henchi et al. [34] is also depicted. The figure shows a good agreement between the finite element solution of the present work with the result obtained by the dynamic stiffness matrix method of Ref. [34].

#### 4.2. Effect of material inhomogeneity

In Fig. 4 the time histories for mid-span deflection of the type A beam with  $\alpha = 0.5$  are depicted for various values of the index  $n$  and two values of the speed parameter,  $f_v = 1/8$  and  $f_v = 1/4$ . At a given value of the moving speed, the dynamic deflection of the beam, as seen from the figure, is greatly influenced by the material parameter  $n$ . The maximum dynamic deflection of the beam steadily increases when raising the index  $n$ , regardless of the moving speed. This can be explained by the fact that, as seen from Eq. (1), the beam with a higher index  $n$  contains more steel, and thus it is softer. The increase in the maximum mid-span dynamic deflection is also clearly seen from Fig. 5, where the deflection factor  $f_D$  is shown as a function of the speed parameter  $f_v$  for various values of the index  $n$ .

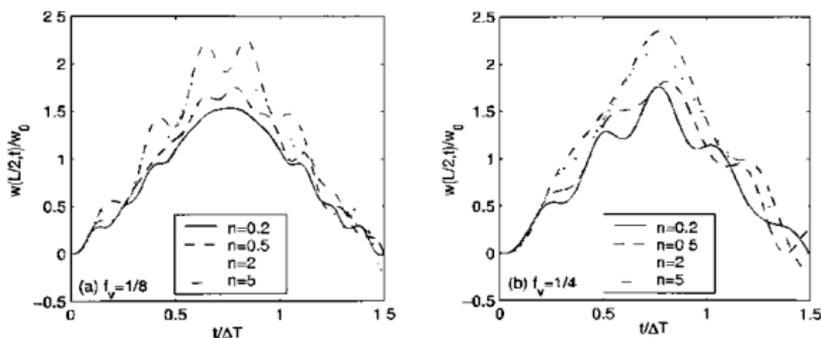


Fig. 4. Time histories for mid-span deflection of type A beam under three moving forces ( $\alpha = 0.5$ ,  $d = L/4$ )

In Fig. 6, the distribution through the beam thickness of the axial stress at the mid-span section is depicted for different values of the index  $n$  and two values of the speed parameter,  $f_v = 1/8$  and  $f_v = 1/4$ . The axial stress shown in the figure was normalized by the maximum static axial stress of a uniform steel beam,  $\sigma_0 = P_0 L h / 8 I_0$ , and it was computed at the time when the second force arrives at the midpoint of the beam. As seen from the figure, the axial stress distribution of the FGM beam is very different from that of the homogeneous beam. The stress of the FGM beam is not symmetrical with regard to the coordinate origin, and it does not become zero on the mid-plane, regardless of

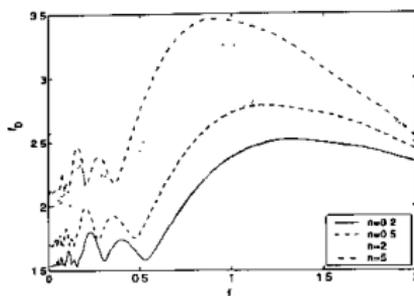


Fig. 5. Speed parameter versus deflection factor of type A beam subjected to three moving forces ( $\alpha = 0.5$ ,  $d = L/4$ )

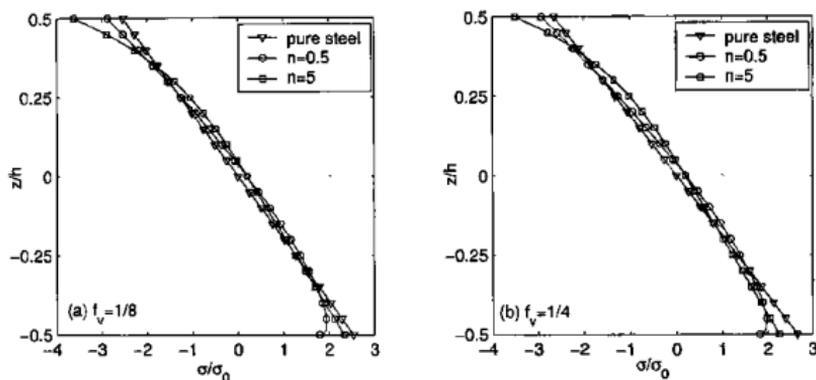


Fig. 6. Normalized axial stress distribution through the thickness of type A beam subjected to three moving forces ( $\alpha = 0.5$ ,  $d = L/8$ )

the moving speed. The moving speed slightly alters the amplitude of the stress, but it hardly changes the distribution of the stress.

#### 4.3. Effect of moving speed

The influence of the moving speed on the dynamic deflection factor of the FGM beam is clearly seen from Fig. 5. For lower values of the speed parameter  $f_v$ , the deflection factor in Fig. 5 both increases and decreases with increasing  $f_v$ , and this phenomenon is associated with the oscillations of the beam when it subjected to a low speed moving load [36]. For higher values of  $f_v$ , as in case of homogeneous beams, the deflection factor increases when raising the speed parameter  $f_v$ , it then reaches a maximum value before decreases. The effect of the moving speed can also be seen from the time histories for the

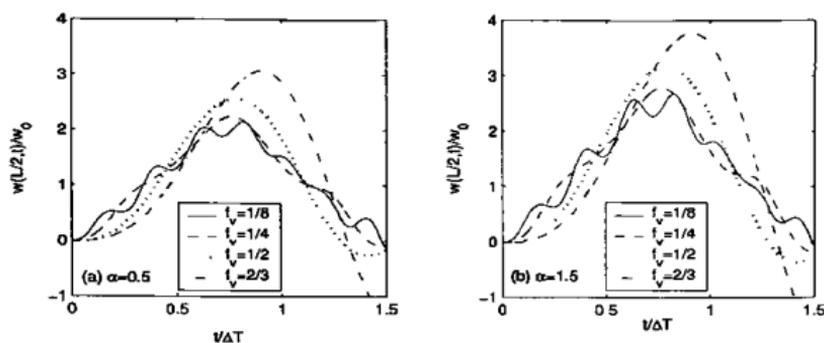


Fig. 7. Time histories for mid-span deflection of type A beam under different speeds moving point forces ( $n = 3, d = L/4$ )

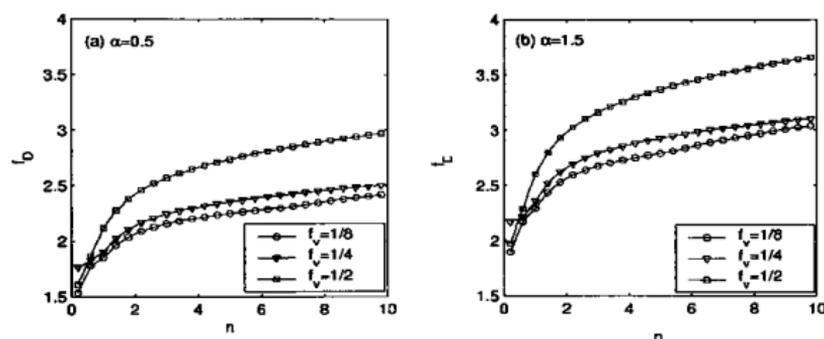


Fig. 8. Material index  $n$  versus deflection factor  $f_D$  of type A beam subjected to three moving forces ( $d = L/4$ )

mid-span deflection and the relation between the deflection factor  $f_D$  and the index  $n$  as depicted in Fig. 7 and Fig. 8 for the type A beam, respectively.

#### 4.4. Effect of distance between the forces

In Fig. 9, the relation between the deflection factor  $f_D$  and the moving speed parameter  $f_b$  of the type A beam with  $n = 0.5$  is shown for various values of the distance between the forces  $d$  and the section parameter  $\alpha$ . The effect of the distance between the forces is clearly seen from the figure, where the deflection factor  $f_D$  is remarkably lower for a smaller distance  $d$ , regardless of the speed and section parameters. The similar situation is occurred for the axial stress as depicted in Fig. 10, where the distribution of the stress through the beam thickness is shown for the type A beam with an index  $n = 0.5$ .

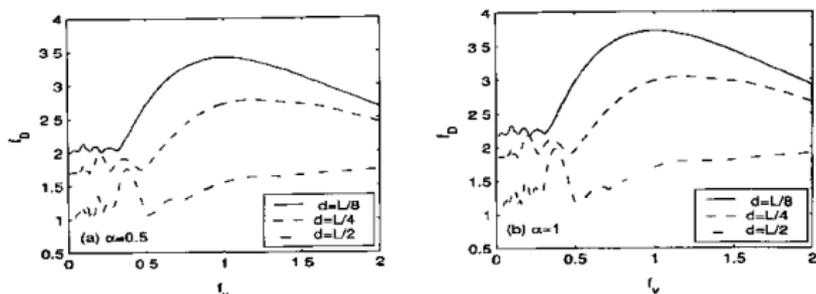


Fig. 9. Effect of distance between moving forces on relation between deflection factor and speed parameter of type A beam ( $n = 0.5$ )

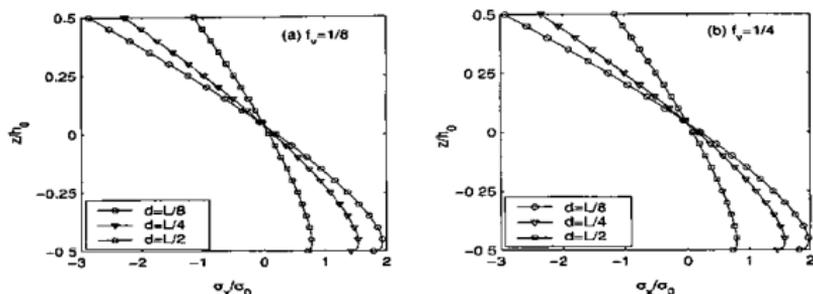


Fig. 10. Effect of distance between moving forces on thickness distribution of axial stress of type A beam ( $n = 0.5$ )

The axial stress increases considerably when the distance between the forces is smaller, regardless of the moving speed.

#### 4.5. Effect of section profile

In Tab. 4 the maximum values of the dynamic deflection factor of the FGM beam subjected to three moving forces are listed for the two types of the section profile, and for various values of the section parameter  $\alpha$  and the index  $n$ . The maximum deflection factor listed in the table increases by raising the section parameter  $\alpha$ , regardless of the section type and the index  $n$ . The maximum deflection factor of the type A beam, as seen from the table, is much more sensitive to the change in the section parameter  $\alpha$  compares to that of the type B beam. For example, with  $n = 3$  the maximum deflection factor of the type A beam increases 18.07% when raising the section parameter from 0 to 1.2, while this value is just 3.54% for the type B beam. The effect of the section profile on the dynamic response of the FGM beam can also be seen from the relation between the

deflection factor  $f_D$  and the index  $n$  as shown in Fig. 11 for two values of the distance between the forces,  $d = L/8$  and  $d = L/4$ . The sensitivity of the type A beam with the change in the section parameter is again clearly observed from the figure.

Table 4. Maximum dynamic deflection factor,  $\max(f_D)$ , for FGM beam with different section profiles subjected to three moving forces ( $d = L/8$ )

Section	$n$	0	0.2	0.4	0.6	0.8	1	1.2
Type A	0.2	2.8729	2.9535	3.0417	3.1388	3.2467	3.3680	3.5064
	0.5	3.1776	3.2668	3.3643	3.4717	3.5911	3.7253	3.8784
	3	3.8203	3.9276	4.0448	4.1740	4.3175	4.4788	4.6629
	5	3.9509	4.0618	4.1830	4.3166	4.4650	4.6318	4.8222
Type B	0.2	2.8729	2.8891	2.9058	2.9231	2.9409	2.9594	2.9785
	0.5	3.1956	3.2140	3.2331	3.2528	3.2732	3.2944	3.3163
	3	3.8203	3.8419	3.8642	3.8871	3.9108	3.9353	3.9607
	5	3.9509	3.9732	3.9962	4.0199	4.0444	4.0698	4.0961

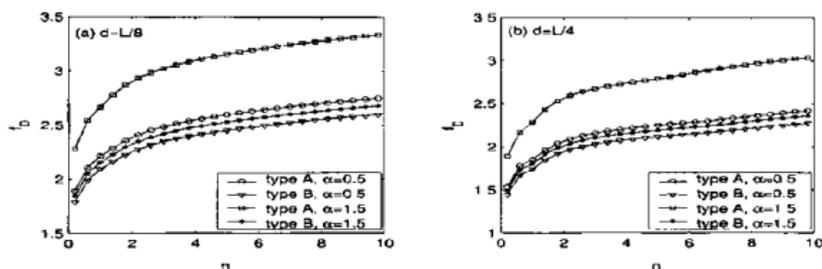


Fig. 11. Relation between deflection factor and material index of FGM beam with different section profiles under three moving forces ( $f_v = 0.5$ )

#### 4.6. Effect of different force numbers

The time histories for the mid-span deflection of type A beam subjected to different numbers of moving forces are shown in Fig. 12 for  $n = 3$ ,  $\alpha = 0.5$ ,  $d = L/4$ , and for two values of the speed parameter,  $f_v = 1/8$  and  $f_v = 1/4$ . As expected, the maximum mid-span dynamic deflection, as seen from Fig. 12, increases when the beam subjected to more numbers of the moving forces. The number of the forces also changes the time at which the maximum mid-span deflection occurs. The relation between the dynamic deflection factor and the moving speed parameter depicted in Fig. 13 for the type A beam with  $n = 3$  and  $\alpha = 0.5$  under different numbers of the moving forces also clearly shows the increase in the deflection factor when the beam subjected to more numbers of the moving forces.

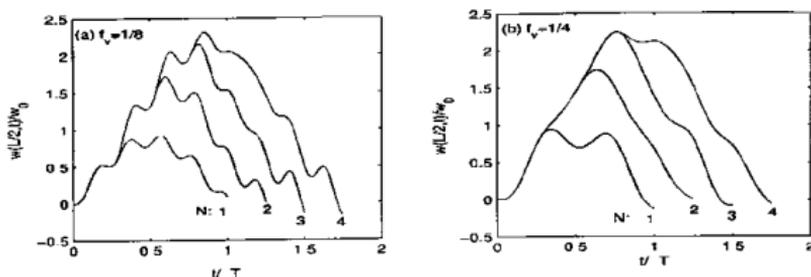


Fig. 12. Time histories for mid-span deflection of type A beam subjected to different numbers of moving forces ( $n = 3, \alpha = 0.5, d = L/4$ )

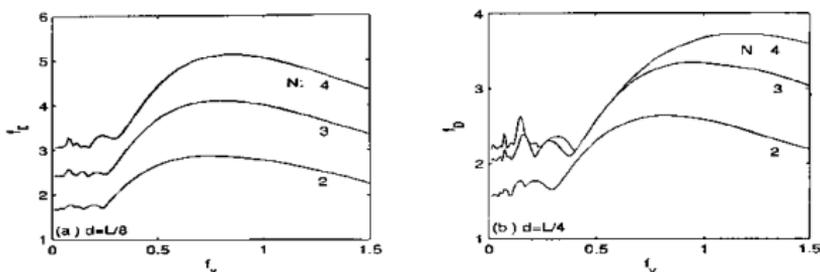


Fig. 13. Relation between deflection factor and speed parameter of type A beam subjected to different numbers of moving forces ( $n = 3, \alpha = 0.5$ )

## 5. CONCLUSIONS

The dynamic behavior of nonuniform FGM Euler-Bernoulli beams subjected to multiple moving forces has been studied by using the finite element method. The material properties of the beams are assumed to vary in the thickness direction by a power law function. A finite element formulation, taking the effect of the cross-section variation and the material inhomogeneity into account, has been derived and employed in the study. The exact variation of the section profile was used in evaluation of the element formulation. The dynamic response of the beam was computed with the aid of the implicit Newmark method. The numerical results have shown that the derived element formulation is accurate in evaluating the dynamic response of the beams. The dynamic characteristics, including the time history, dynamic deflection factor, axial stress distribution are governed by the moving speed, section profile, number of forces as well as the distance between the forces. A parametric study has been carried out to highlight the influence of the material inhomogeneity, section profile and loading parameters on the dynamic behavior of the nonuniform FGM beams under the moving forces.

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